# Piezoelectric properties of $MnO_2$ doped low temperature sintering $Pb(Mn_{1/3}Nb_{2/3})O_3-Pb(Ni_{1/3}Nb_{2/3})O_3-Pb$ $(Zr_{0.50}Ti_{0.50})O_3$ ceramics

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Abstract In this study, in order to develop the composition ceramics for low loss and low temperature sintering multilayer piezoelectric actuator, Pb(Mn<sub>1/3</sub>Nb<sub>2/3</sub>)O<sub>3</sub>-Pb  $(Ni_{1/3}Nb_{2/3})O_3\text{--}Pb(Zr_{0.50}Ti_{0.50})O_3$  (abbreviated as PMN-PNN-PZT) ceramics were fabricated using Li<sub>2</sub>CO<sub>3</sub> and Na<sub>2</sub>CO<sub>3</sub> as sintering aids, and their piezoelectric and dielectric characteristics were investigated according to the amount of MnO2 addition. At the 0.2 wt% MnO2 doped specimen sintered at 900 °C, density and mechanical quality factor  $(Q_m)$  showed the maximum values of 7.81 [g/cm<sup>3</sup>]and 1186, respectively. And also, at 0.1 wt% MnO<sub>2</sub> doped specimen, electromechanical coupling factor  $(k_{\rm p})$ , piezoelectric constant  $(d_{33})$  of specimen showed the maximum values of 0.608 and 377[pC/N], respectively. Dielectric constant ( $\varepsilon_r$ ) slightly decreased with increasing  $MnO_2$ . Taking into consideration the density of 7.81[g/cm<sup>3</sup>], electromechanical coupling factor  $(k_p)$  of 0.597 the mechanical quality factor  $(Q_m)$  of 1,186, and piezoelectric constant  $(d_{33})$  of 356[pC/N], it could be concluded that 0.2 wt% MnO<sub>2</sub> doped composition ceramics sintered at 900 °C was best for low loss and low temperature sintering multilayer piezoelectric actuator application.

**Keywords** Low loss multilayer piezoelectric actuator · Low temperature sintering · Mechanical quality factor · Electromechanical coupling factor

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#### **1** Introduction

Piezoelectric actuators has been widely utilized for the applications as optical instrument, precision machine, miniature motor and mobile instrument because they have the merits such as high force per unit volume, rapid response velocity, precision position control and miniaturization [1, 2].

Piezoelectric actuator requires high electromechanical coupling factor  $(k_p)$  and piezoelectric constant  $(d_{33})$  in order to induce a large strain in proportional to applied electric field. Therefore, multilayer structured piezoelectric actuators have been suggested to increase output displacements. And also, to prevent its heat generation, when it is driven with high voltage for a long time, high mechanical quality factor  $(Q_m)$  is required.

In general, PZT system ceramics should be sintered at high temperatures between 1200 and 1300 °C in order to obtain complete densification. Accordingly, environmental pollution due to its PbO evaporation and the use of expansive Pd rich Ag/Pd internal electrode in case of manufacturing multilayer ceramic actuator are inevitable. Hence, to reduce its sintering temperature, various kinds of material processing methods such as hot pressing, high energy mill, liquid phase sintering, and using ultra fine powder have been performed. Among these methods, liquid phase sintering is basically an effective method for aiding densification at low temperature. The theoretical explanation for liquid phase sintering was already reported over 40 years ago [3].

Hence, in this study, in order to develop low loss and low temperature sintering composition ceramics for multilayer actuator application, PMN-PNN-PZT ceramics were fabricated using  $Li_2CO_3$  and  $Na_2CO_3$  as sintering aids [4, 5] and their piezoelectric and dielectric properties were investigated according to the amount of  $MnO_2$  addition.



Fig. 1 X-ray diffraction pattern of specimens according to the amount of  $MnO_2$  addition

### 2 Experimental

The specimens were manufactured using a conventional mixed oxide process. The compositions used in this study were as follows;

$$Pb(Mn_{1/3}Nb_{2/3})_{0.02}(Ni_{1/3}Nb_{2/3})_{0.12}(Zr_{0.50}Ti_{0.50})_{0.86}O_3 + Xwt\% MnO_2 + sintering aids(0.2 wt\% Na_2CO_3 + 0.2 wt\% Li_2CO_3)$$

(X = 0, 0.1, 0.2, 0.3, 0.4, 0.5).

The raw materials such as PbO,  $ZrO_2$ ,  $TiO_2$ ,  $MnO_2$ ,  $Nb_2O_5$  and NiO for the given composition were weighted by mole ratio and the powders were ball-milled for 24 h. After drying, they were calcined at 850 °C for 2 h. Thereafter,  $Na_2CO_3$  and  $Li_2CO_3$  were added, ball-milled, and dried again. A polyvinyl alcohol (PVA: 5 wt% aqueous solution) was added to the dried powders. The powders

were molded by the pressure of 1,000 kg/cm<sup>2</sup> in a mold which has a diameter of 21 mm, burned out at 600 °C for 3 h, and then sintered at 900 °C for 2 h. For measuring the piezoelectric characteristics, the specimens were polished to 1 mm thickness and then electrodeposited with Ag paste. Poling was carried out at 120 °C in a silicon oil bath by applying fields of 30 kV/cm for 30 min. All the samples were aged for 24 h prior to measuring the piezoelectric and dielectric properties. For investigating the dielectric properties, capacitance was measured at 1 kHz using an LCR meter (ANDO AG-4034) and dielectric constant ( $\varepsilon_r$ ) was calculated. For investigating the piezoelectric properties, the resonant and anti-resonant frequencies were measured by an Impedance Analyzer (Agilent 4294A) according to IEEE standard and then the  $k_p$  and  $Q_m$  were calculated.

#### **3** Results and discussion

Figure 1 shows X-ray diffraction pattern of specimens according to the amount of  $MnO_2$  addition. All the specimens showed tetragonal structure and included secondary phase. With increasing the amount of  $MnO_2$ addition, tetragonality (c/a) increased as shown in Table 1. This phenomenon can be illustrated as general hardener doping effect in the Pb(Zr,Ti)O\_3 system ceramics. On the other hand, secondary phases were decreased, with increasing the amount of  $MnO_2$  addition. It seemed that  $MnO_2$ doping enhanced sinterability of Pb( $Mn_{1/3}Nb_{2/3}$ )<sub>0.02</sub>( $Ni_{1/3}Nb_{2/3}$ )<sub>0.12</sub>( $Zr_{0.50}Ti_{0.50}$ )<sub>0.86</sub>O<sub>3</sub> system ceramics due to the increase of oxygen vacancies. That is, the oxygen vacancies promote lattice diffusion, thereby assisting the process of sintering and grain growth.

Figure 2 shows microstructure of fractured surface according to the amount of  $MnO_2$  addition. The linear intercept method was used to measure the grain size. At 0.1 wt%  $MnO_2$  doped specimen, grain size increased more or less up to 2.95  $\mu$ m compared with 2.63  $\mu$ m of non doped specimen. And the composition ceramics more than 0.1 wt %  $MnO_2$  doping, it was nearly saturated. This result can be also explained by the improvement of sinterability.

Table 1 Physical characteristic of specimens according to the amount of MnO<sub>2</sub> addition.

Sintering temp. (°C)	MnO <sub>2</sub> addition (wt%)	Density (g/cm <sup>3</sup> )	$\mathcal{E}_{\mathrm{r}}$	k <sub>p</sub>	$Q_{\rm m}$	<i>d</i> <sub>33</sub> (pC/N)	Tetragonality (c/a)	Curie temp. (°C)
900	0	7.807	1144	0.546	473	355	1.0089	355
	0.1	7.812	1010	0.608	980	377	1.0089	376
	0.2	7.816	920	0.597	1186	356	1.0098	371
	0.3	7.817	864	0.582	1032	320	1.0120	370
	0.4	7.815	810	0.570	980	300	1.0128	372
	0.5	7.815	788	0.564	776	293	1.0159	371

Fig. 2 (a)–(d) Microstructure of specimens according to the amount of  $MnO_2$  addition



Figure 3 shows density of specimens according to the amount of  $MnO_2$  addition. All the specimens were fully densified due to the liquid phase sintering. Eutectic temperature of Li<sub>2</sub>CO<sub>3</sub> and Na<sub>2</sub>CO<sub>3</sub> compound is about 514 °C. At the temperature, liquid phase is started and helps densification of specimens at low temperature. With increasing the amount of  $MnO_2$  addition, density increased up to

 $0.3 \text{ wt\% MnO}_2$  and then decreased. It is clear evidence that  $MnO_2$  enhances sinterability of the composition.

Figure 4 shows dielectric constant ( $\varepsilon_r$ ) of specimens according to the amount of MnO<sub>2</sub> addition. With increasing the amount of MnO<sub>2</sub> addition,  $\varepsilon_r$  linearly decreased because movement of domain is not feasible due to the hardener doping effect.



Fig. 3 Density of specimens according to the amount of  $\mbox{MnO}_2$  addition



Fig. 4 Dielectric constant( $\varepsilon_r$ ) of specimens according to the amount of MnO<sub>2</sub> addition



Fig. 5 Electromechanical coupling factor  $(k_p)$  of specimens according to the amount of MnO<sub>2</sub> addition



Figure 6 shows piezoelectric  $d_{33}$  constant of specimens according to the amount of MnO<sub>2</sub> addition. The variation of  $d_{33}$  also coincided with the trend of  $k_p$ , and a maximum



Fig. 7 Mechanical quality factor  $(Q_m)$  of specimens according to the amount of MnO<sub>2</sub> addition

value of it shows 377[pC/N] at 0.1 wt% MnO<sub>2</sub> added specimen.

Figure 7 shows  $Q_m$  of specimens according to the amount of MnO<sub>2</sub> addition. With increasing the amount of MnO<sub>2</sub> addition,  $Q_m$  increased at 0.2 wt% MnO<sub>2</sub> added specimen and then decreased. This result can be explained by the fact that oxygen vacancies are created due to the accepter doping effect. That is, it is well-known that manganese mainly coexists in the Mn<sup>2+</sup> and Mn<sup>3+</sup> states in PZT systems, which enter into lattice structure in order to substitute Ti<sup>4+</sup> and Zr<sup>4+</sup> ion, thus the unbalance of valence led to the creation of oxygen vacancies. The oxygen vacancies cause the increase of  $Q_m$ . The maximum value of  $Q_m$  showed 1,186 at 0.2 wt% MnO<sub>2</sub> added specimen.



18000 □-0wt% MnO. 16000 -0-0.2wt% MnO △-0.5wt% MnO. 14000 Dielectric constant  $\varepsilon_r$ 12000 10000 8000 6000 4000 2000 0 100 400 150 200 250 300 350 Temperature [°C]

Fig. 6 Piezoelectric constant  $(d_{33})$  of specimens according to the amount of MnO<sub>2</sub> addition

Fig. 8 Temperature dependence of dielectric constant of specimen according to the amount of  $MnO_2$  addition



Fig. 9 Hysteresis curves of non doped and 0.2 wt%  $MnO_2$  doped specimens

Figure 8 shows temperature dependence of dielectric constant of the  $MnO_2$  doped specimen. Curie temperature increased up to 0.1 wt%  $MnO_2$ . And the composition ceramics more than 0.1 wt%  $MnO_2$  addition, it was nearly saturated as about 370–372 °C.

Figure 9 shows hysteresis curve of non doped and 0.2 wt %  $MnO_2$  doped specimen, respectively. Remanent polarization(Pr) and coercive field(Ec) of 0.2 wt%  $MnO_2$  added specimen showed higher values than those of non doped one more or less. Above results could be also explained by the facts that Pr and Ec were simultaneously increased by virtue of the enhancement of sinterability and hardener doping effect due to  $MnO_2$  doping.

Table 1 shows physical characteristics of specimens according to the amount of  $MnO_2$  addition.

## **4** Conclusions

In this study, in order to develop low loss and low temperature sintering composition ceramics for multilayer actuator application, PMN-PNN-PZT ceramics were fabricated using Li<sub>2</sub>CO<sub>3</sub> and Na<sub>2</sub>CO<sub>3</sub> as sintering aids and their piezoelectric and dielectric properties were investigated according to the amount of MnO<sub>2</sub> addition. The results obtained from the experiment are as follow:

- 1. All the specimens were densified at sintering temperature of 900 °C by sintering aids and MnO<sub>2</sub> addition enhanced sinterability of specimens. With increasing the amount of MnO<sub>2</sub> addition, dielectric constant ( $\varepsilon_r$ ) rapidly decreased.
- At 0.1 wt% MnO<sub>2</sub> added specimen, k<sub>p</sub> and d<sub>33</sub> showed the maximum value of 0.608 and 377[pC/N], respectively
- 3. At 0.2 wt% MnO<sub>2</sub> added specimen,  $Q_{\rm m}$  showed the maximum value of 1186.

At 0.2 wt% MnO<sub>2</sub> added specimen, density,  $\varepsilon_r$ ,  $k_p$ ,  $Q_m$  and  $d_{33}$  showed optimum value of 7.816[g/cm<sup>3</sup>], 920, 0.597, 1186 and 356[p/CN], respectively for low loss and low temperature sintering multilayer piezoelectric actuator application.

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